IRON-COPPER ELECTRODES FOR ALKALINE BATTERIES

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Alkaline Ni-Fe batteries employ sintered iron electrodes as anodes. Iron oxide and copper powders are added to iron powder during sintering to improve charge retention and cycle life. Electrochemical studies on the iron-copper electrodes revealed that iron oxide addition hindered the formation of higher valent oxides of iron and reduced the self discharge. An optimum composition of iron oxide and copper for iron electrodes has been suggested.

Keywords: Nickel-iron battery, sintered iron electrode, alkaline iron electrode and iron-copper electrode

INTRODUCTION

Sintered porous iron electrodes are used in the Ni-Fe cell to have long cycle life. To increase the hardness strength and conductivity, copper powder is incorporated in the sintered iron electrode [1]. Inclusion of copper powder favours uniform pore size distribution and lowers the sintering temperature of the electrode [2,3]. When copper is added up to 20%, pressed Fe(III) oxides exhibited better utilisation. The present work is aimed to understand the electrochemical behaviour of sintered Fe-Cu electrodes in 6.0 M KOH + 0.63 MLiOH with a view to develop a battery electrode with high charge retention.

EXPERIMENTAL DETAILS

Preparation of porous iron electrode

Iron powders of different origins with different properties were used for the electrode preparation (Table I). Iron powder was reduced at 573 K for two hours in hydrogen atmosphere. Loose sintered electrodes were prepared from iron powder and the mixtures of Fe, Fe₃O₄ and Cu using a number 10 nickel mesh grid of 0.1 mm thick (area 1.67 cm², thickness - 2mm) in a graphite die. The electrode was sintered at 1173K for one hour in N₂ atmosphere. The amounts of Fe²⁺ and Fe³⁺ ions in Fe₃O₄ were estimated [4]. Details of the experimental setup for triangular potential sweep voltammetry (TPSV) and gasometric studies have been described earlier [5].

Potential step method and solution analysis

The electrodes were kept at constant potential -0.9, -0.775, -0.525 and -0.29 V for one hour. After the experiments the solutions were analysed using atomic absorption spectrophotometer (Perkin Elmer 380, USA).

Experiments in duplicate were carried out at 303 ± 0.01 K using analar chemicals dissolved in double distilled water. The electrolyte 6 M KOH + 0.63 MLiOH was deoxygenated by bubbling purified H₂ for one hour. Potentials were measured against Hg/HgO electrode and no corrections were made for liquid junction potentials.

RESULTS

A porous (Fe + 3% Cu) electrode was kept at -1.3 V for 5 min., disconnected, shaken free of attached H₂ bubbles and then polarised from -1.3V to -0.2V (Fig. 1). In the forward scan ZCCP (Zero current crossing potential) occurs at -1.03 V followed by a plateau around -0.9V (I), an anodic peak at -0.825V (II), a shoulder around -0.7V (III), a peak at -0.64V (II) a complete passive region from -0.56V to -0.42V (V) and a sharp peak at 0.325V (VI). The backward scan exhibits a passive region from -0.2V to -0.55V a sharp peak at -0.94 V (VIII) and peak at -1.1V (IX). Hydrogen evolution was noticed at -1.2V. Increase of scan number reduces the amounts of charge under peaks II, IV and IX increases those for VI, VII and VIII.

This suggests that peaks II and IX belong to a redox couple while the peaks VI, VII and VIII are consecutive.

Introduction of Fe₃O₄ to this electrode slightly modified the spectrum (Fig. 2). During the forward scan ZCCP occurs at -1.035V followed by a plateau around -1.0V (I) and anodic peaks at -0.8V (II), -0.58V (III) and -0.325V (IV). During the reverse scan cathodic peaks appear at -0.75V (V), -0.975 V (VI) and -1.140V (VII). Hydrogen evolution takes place at -1.225V. On repeating the polarisation for a few more cycles the reversibility was found to be increased.
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<table>
<thead>
<tr>
<th>Powder</th>
<th>Chemical composition</th>
<th>Apparent density g/cc</th>
<th>Tap density g/cc</th>
<th>Particle size</th>
<th>Specific area* m²/g</th>
</tr>
</thead>
<tbody>
<tr>
<td>Electrolytic iron</td>
<td>99% Fe, 0.001% Pb, 0.008% Zn, 0.001% As, 0.025% Mn, 0.005% Cu</td>
<td>2.84</td>
<td>3.08</td>
<td>≤ 37</td>
<td>11.08</td>
</tr>
<tr>
<td>Water atomised iron (ASC 200)</td>
<td>98% Fe, 0.01 % C, 0.007% S, 0.007% P</td>
<td>2.8 to 3.0</td>
<td>—</td>
<td>92%</td>
<td>18.52</td>
</tr>
<tr>
<td>Sponge iron (MH 300.25)</td>
<td>98% Fe, 0.01% C, 0.007% S, 0.007% P</td>
<td>2.75 to 2.95</td>
<td>—</td>
<td>≤ 44% and 20%</td>
<td>14.00</td>
</tr>
<tr>
<td>Synthetic black iron oxide Fe₂O₄</td>
<td>96 to 99% Fe₂O₄, Fe²⁺ = 44.55%, Fe³⁺ = 25.73%</td>
<td>1.22</td>
<td>1.71</td>
<td>≤ 37</td>
<td>38.72</td>
</tr>
<tr>
<td>Electrolytic copper</td>
<td>99.5% Cu</td>
<td>—</td>
<td>—</td>
<td>≤ 37</td>
<td>14.21</td>
</tr>
</tbody>
</table>

* Quantasorb using liquid N₂

Gasometric studies

The self discharge of the iron electrode is caused by local action accompanied by H₂ evolution. The self discharge current was calculated from the rate of H₂ evolution. The electrode was polarised cathodically at five different potentials and the rate of H₂ evolution was monitored. The

\[ \text{Fig. 1: Typical cyclic voltammogram for porous electrolytic iron powder + 3% Cu electrode in} \]
\[ 6 \text{ M KOH + 0.63 M LiOH solutions with various scan numbers} \]
\[ E_{\text{on}} = -1.3 \text{v; } E_{\text{off}} = -0.2 \text{v; } v = 1 \text{ mVs}^{-1} \]
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linear segment of the polarisation curve was extrapolated to open circuit potential to obtain self discharge current (Fig. 3).

**DISCUSSION**

Oxidation - reduction processes occurring at the iron electrode surface was reviewed recently [6]. The formation of Fe(OH)₃ takes place via FeOH⁺ ads and the further oxidation of Fe(OH)₃ to FeOOH can take place as [7,8], Fe(OH)₂ + OH⁻ → FeOOH + H₂O + e⁻. In 6 M KOH solution, HFeO₂⁻ formation is also envisaged as Fe(OH)₂ may be formed via dissolution - precipitation.

The appearance of a plateau around -1.0V is due to the initial oxidation on the surface. The appearance of peak at -0.825V (II) is due to the formation of Fe(OH)₂ or HFeO₂⁻ ion.

The shoulder around -0.7V (III) appears anodic to the E_c of Cu/Cu₂O reaction [9].

\[
\begin{align*}
\text{Cu} + 2\text{H}_2\text{O} & \rightarrow \text{CuO}_2^{2⁻} + 4\text{H}⁺ + 2e⁻ \\
E_c & = -1.136 \text{ V vs Hg/HgO} \\
\text{Cu}⁺ + 2\text{H}_2\text{O} & \rightarrow \text{HCuO}_2^{2⁻} + 3\text{H}⁺ + e⁻ \\
E_c & = -1.026 \text{ V vs Hg/HgO}
\end{align*}
\]

Hence it may be due to the dissolution of Cu via monovalent oxide along with Fe(OH)₂.

In order to confirm the dissolution of Cu, an analysis of the solution was carried out at different potentials. Anodic potentials increased the copper ion concentration in solution, while iron content decreased (Table II). Dissolved copper ions were observed only at potentials anodic to -0.775V. The appearance of peak (IV) is due to the complete oxidation of Fe(OH)₂ to FeOOH.

Oxidation of copper can occur [10] in two stages with two surface films of distinctly different morphologies and growth mechanisms. A compact layer is formed by solid state growth mechanism followed by the nucleation and growth of the upper layer of individual crystals from solutions. Copper can dissolve at 0.77V to give HCuO₂⁻.

The appearance of the passive region around -0.5V (V) is due to the formation of the base layer of Cu₂O via

\[
\begin{align*}
\text{Cu} & \rightarrow \text{Cu}^{⁺} \text{ads} + e⁻ \\
2\text{Cu}^{⁺} \text{ads} & \rightarrow 2\text{Cu}^{oxide} \\
\text{OH}⁻ \text{solution} & \rightarrow \text{OH}^{ads} \\
\text{OH}^{ads} & \rightarrow \text{O}^{2⁻} \text{oxide lattice} + \text{H}^{⁺} \text{solution} \\
2\text{Cu}^{⁺} \text{oxide lattice} + \text{O}^{2⁻} \text{oxide lattice} + \text{H}^{⁺} \text{solution} & \rightarrow \text{Cu}_2\text{O}
\end{align*}
\]

The monovalent Cu⁺ may be present on the pores of the oxide and react with OH⁻ ions to form Cu₂O.

\[
\begin{align*}
\text{OH}⁻ \text{solution} & \rightarrow \text{OH}^{ads} \\
\text{OH}^{ads} & \rightarrow \text{O}^{2⁻} \text{oxide lattice} + \text{H}^{⁺} \text{solution} \\
2\text{Cu}^{⁺} \text{oxide lattice} + \text{O}^{2⁻} \text{oxide lattice} + \text{H}^{⁺} \text{solution} & \rightarrow \text{Cu}_2\text{O}
\end{align*}
\]

![Fig. 2: Typical cyclic voltammogram for porous electrolytic iron + 15% Fe₃O₄ + 3% Cu electrode in 6 M KOH + 0.63 M LiOH solutions with various scan numbers](image)

\[E_{c,0} = -1.3V; \quad E_{c,4} = -0.2V; \quad v = 1 \text{ mV}s^{-1}\]
This strongly bound layer completely covers the pores of the oxide surface. At potentials -0.4V some part of the Cu$_2$O may dissolve to yield [Cu(OH)$_2$]$^{2-}$ (peak VI).

In the reverse scan the entire surface is covered by Cu$_2$O while at a potential of -0.6V the appearance of peak VII is due to the irreversible reduction of oxides of copper. The appearance of cathodic peaks at -0.94V (VIII) and peak (IX) at -1.10V is due to the reduction of FeOOH to Fe(OH)$_2$ and then to iron. At high sweep rates, the surface of the electrode participates predominantly in the electrode process. The reduction to copper can also occur from soluble Cu(OH)$_2$$^{2-}$ at higher cathodic potentials.

$$[\text{Cu(OH)}_2]^ {2-}_{\text{solution}} \rightarrow \text{Cu}_2\text{O} + (n-2) \text{OH}^- + \text{H}_2\text{O}$$

and

$$\text{Cu}_2\text{O} + \text{H}_2\text{O} + 2e^- \rightarrow 2\text{Cu} + 2\text{OH}^-$$

The freshly precipitated ‘active’ copper surface causes a rise in potential for H$_2$ evolution.

Introduction of Fe$_3$O$_4$ to (Fe + 3% Cu) electrode caused the disappearance of peak (III) (ill-defined in Fig. 1). This suggests that the oxidation of Cu to Cu$_2$O is hindered. The peak potential (IV) was shifted to more noble values. Increase of oxide content enhanced the over-voltage for the process of conversion of Fe(OH)$_2$ to FeOOH. The reason for this retardation could be that Fe$_3$O$_4$ is in redox equilibrium with the newly formed Fe(OH)$_2$:

as

$$\text{Fe}_3\text{O}_4 + 2\text{H}_2\text{O} + 2e^- \rightarrow \text{Fe(OH)}_2 + 2\text{FeO} + 2\text{OH}^-$$

The presence of Fe$_3$O$_4$ reduced the charges flowed under peak V suggesting that the dissolution as divalent soluble Cu is hindered.

Criteria for a battery electrode

The ideal battery electrode requires the reaction

$$\text{Fe(OH)}_2 + 2e^- \rightarrow \text{Fe} + 2\text{OH}^-$$

to proceed reversibly. In TPSV studies the appearance of an anodic peak (II) and the cathodic peak (IX) corresponds to Fe/Fe (II) redox couple [11,12].

$$(E_p, \text{II}) - (E_p, \text{IX}) = \Delta E_p$$

Where $\Delta E_p$ is a measure of irreversibility. The more the value of $\Delta E_p$, the more irreversible is the process. As $\Delta E_p$ varied linearly with $v$, the extrapolation of $\Delta E_p$ to zero sweep rate will help in studying the behaviour near reversible potential. An electrode with ($\Delta E_p$)$_{v \rightarrow 0} = 0$ will exhibit maximum reversibility.

The values of $Q_c/Q_a$ correspond to the charge associated with oxide reduction and the formation of Fe/Fe(II) couple.

**TABLE II: Solution analysis for electrolytic iron and electrolytic iron + 3% Cu electrodes in 6 M KOH + 0.6 M LiOH solutions**

<table>
<thead>
<tr>
<th>Potential applied (mV)</th>
<th>Dissolved iron (mg/lit)</th>
<th>Dissolved copper (mg/lit)</th>
</tr>
</thead>
<tbody>
<tr>
<td>-900</td>
<td>2.0</td>
<td>0.0</td>
</tr>
<tr>
<td>-775</td>
<td>1.7</td>
<td>0.0</td>
</tr>
<tr>
<td>-525</td>
<td>1.6</td>
<td>0.6</td>
</tr>
<tr>
<td>-290</td>
<td>1.5</td>
<td>0.8</td>
</tr>
</tbody>
</table>
TABLE III: Parameters derived from TPSV studies —
Effect of source of iron powder, copper and Fe$_3$O$_4$
additions

<table>
<thead>
<tr>
<th>Electrode Composition</th>
<th>Fe/Fe(II) couple</th>
<th>(Δ$E_p$)$_{v 	o 0}$</th>
<th>$Q_c$/$Q_a$</th>
<th>mV</th>
</tr>
</thead>
<tbody>
<tr>
<td>Electrolytic iron + 1% Cu</td>
<td>280</td>
<td>0.92</td>
<td></td>
<td></td>
</tr>
<tr>
<td>+ 2% Cu</td>
<td>300</td>
<td>1.00</td>
<td></td>
<td></td>
</tr>
<tr>
<td>+ 3% Cu</td>
<td>230</td>
<td>1.33</td>
<td></td>
<td></td>
</tr>
<tr>
<td>+ 4% Cu</td>
<td>285</td>
<td>1.44</td>
<td></td>
<td></td>
</tr>
<tr>
<td>+10% Cu</td>
<td>265</td>
<td>1.77</td>
<td></td>
<td></td>
</tr>
<tr>
<td>+15% Cu</td>
<td>280</td>
<td>1.54</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Electrolytic Fe + 3% Cu + 3% Fe$_3$O$_4$</td>
<td>225</td>
<td>0.89</td>
<td></td>
<td></td>
</tr>
<tr>
<td>+ 10% Fe$_3$O$_4$</td>
<td>240</td>
<td>0.88</td>
<td></td>
<td></td>
</tr>
<tr>
<td>+ 15% Fe$_3$O$_4$</td>
<td>305</td>
<td>0.87</td>
<td></td>
<td></td>
</tr>
<tr>
<td>+ 20% Fe$_3$O$_4$</td>
<td>235</td>
<td>1.06</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Sponge Fe + 3% Cu + 15% Fe$_3$O$_4$</td>
<td>270</td>
<td>0.96</td>
<td></td>
<td></td>
</tr>
<tr>
<td>Water atomised Fe + 3% Cu + 15% Fe$_3$O$_4$</td>
<td>295</td>
<td>0.81</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

For iron oxide electrodes containing copper peaks II and VII were used to calculate Δ$E_p$ and $Q_c$/$Q_a$ for reversibility of Fe/Fe(II) redox couple.

Even in solid iron electrodes the values of (Δ$E_p$)$_{v 	o 0}$ for Fe/Fe(II) couple is 275 mV and this amount of irreversibility is always present as the electrode surface is covered by oxides. An electrode which gives (Δ$E_p$)$_{v 	o 0}$ values close to that of 275 mV is considered to be the best.

Addition of 3% copper to the electrolytic iron powder gave a value of 230 mV for (Δ$E_p$)$_{v 	o 0}$ and electrodes prepared from mixtures of electrolytic iron +3% copper with various amounts of Fe$_3$O$_4$ exhibited 205 to 240 mV for (Δ$E_p$)$_{v 	o 0}$ compared to 275 mV obtained for solid iron and thus favour reversibility of Fe $\rightleftharpoons$Fe(OH)$_2$ reaction (Table III). When compared to the 295 mV and 270 mV obtained for electrodes 3% Cu + 15% Fe$_3$O$_4$ containing water atomised powder and sponge iron powders, electrolytic iron powder + 3% Cu + 15% Fe$_3$O$_4$ exhibited 235 mV for (Δ$E_p$)$_{v 	o 0}$.

The self discharge currents of the electrodes prepared from copper and Fe$_3$O$_4$ powders (Table IV) revealed that Fe$_3$O$_4$ addition lowered the self discharge of electrolytic iron powder compared to sponge iron powder electrode. This is because of the reduction in $i_b$ for hydrogen evolution [13]. Addition of copper enhances the self discharge of Fe$_3$O$_4$ electrodes enhancing the dissolution of iron by galvanic action. However the simultaneous addition of Fe$_3$O$_4$ and copper into iron electrodes reduces the self discharge current compared to electrodes from electrolytic iron powder. Sponge iron powder exhibits more self discharge compared to the other electrodes.

TABLE IV: Self discharge current of iron electrode in 6 M KOH + 0.63 M LiOH solutions

<table>
<thead>
<tr>
<th>Electrode composition</th>
<th>* Self discharge current mA/g (±0.1)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Electrolytic iron powder</td>
<td>0.8</td>
</tr>
<tr>
<td>Electrolytic iron powder + 15% Fe$_3$O$_4$</td>
<td>0.2</td>
</tr>
<tr>
<td>Electrolytic iron + 3% Cu</td>
<td>1.1</td>
</tr>
<tr>
<td>Electrolytic iron powder + 15% Fe$_3$O$_4$ + 3% Cu</td>
<td>0.75</td>
</tr>
<tr>
<td>Water atomised iron powder + 15% Fe$_3$O$_4$ + 3% Cu</td>
<td>0.64</td>
</tr>
<tr>
<td>Sponge iron powder + 15% Fe$_3$O$_4$ + 3% Cu</td>
<td>1.61</td>
</tr>
</tbody>
</table>

**CONCLUSION**

Though electrolytic iron powder + 15% Fe$_3$O$_4$ electrodes have the least self discharge current, the electrical conductivity of the electrodes are poor compared to electrodes containing copper powder. Hence electrolytic Fe powder +3% Cu+15% Fe$_3$O$_4$ is the optimum composition for iron electrodes for use in Ni-Fe batteries for enhanced conductivity, cycle life and charve retention.

REFERENCES


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